

Blade Pitch Control for Floating Wind Turbines: Design and Experiments Using a Scale Model

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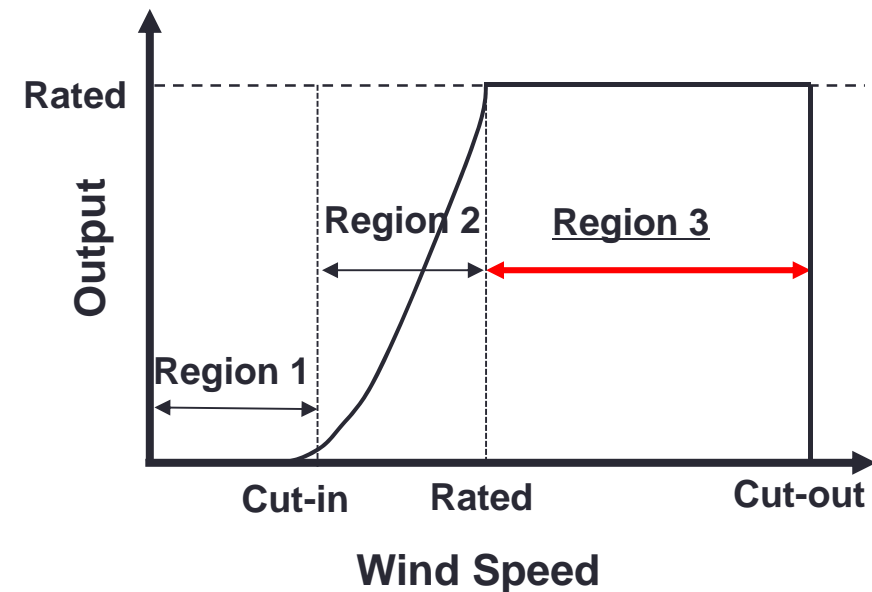
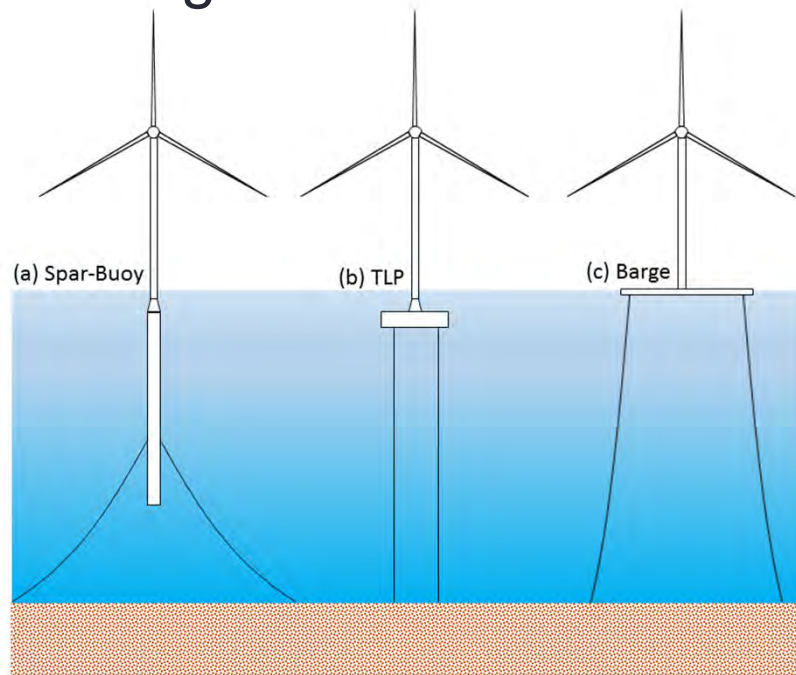
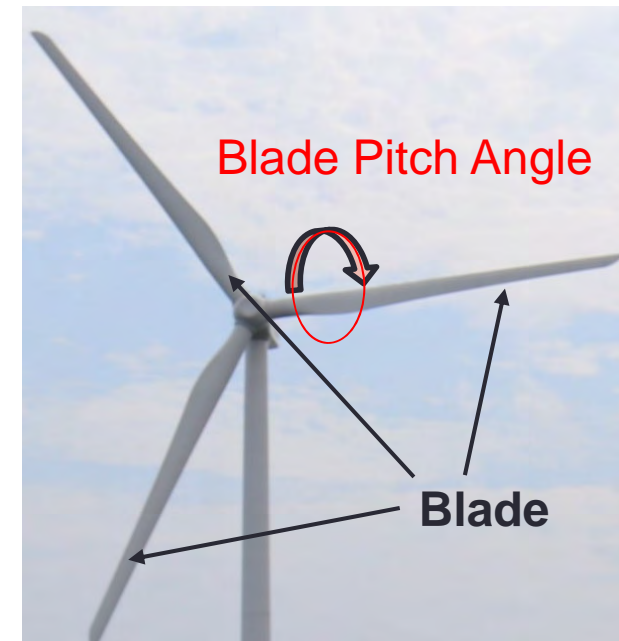
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Introduction

- Blade Pitch Control in Wind Turbines
 - Used in Region 3
 - (main) Objective: keep the power output to the rated value.
- Floating Offshore Wind Turbines



Introduction

- Example of FOWT (Floating Offshore Wind Turbine)

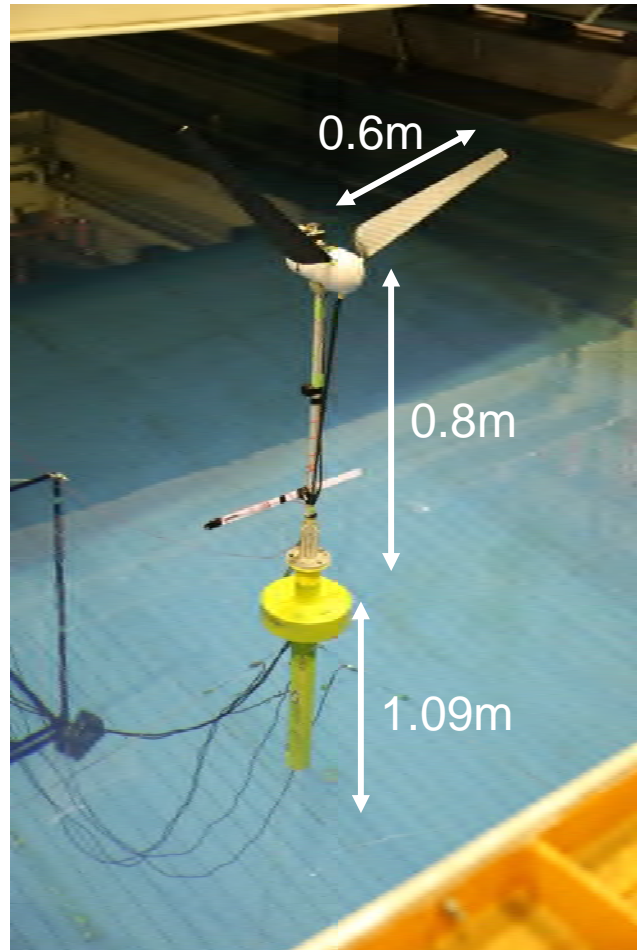
2MW FOWT (spar-buoy type)
Offshore Nagasaki, Japan (August 25, 2014)



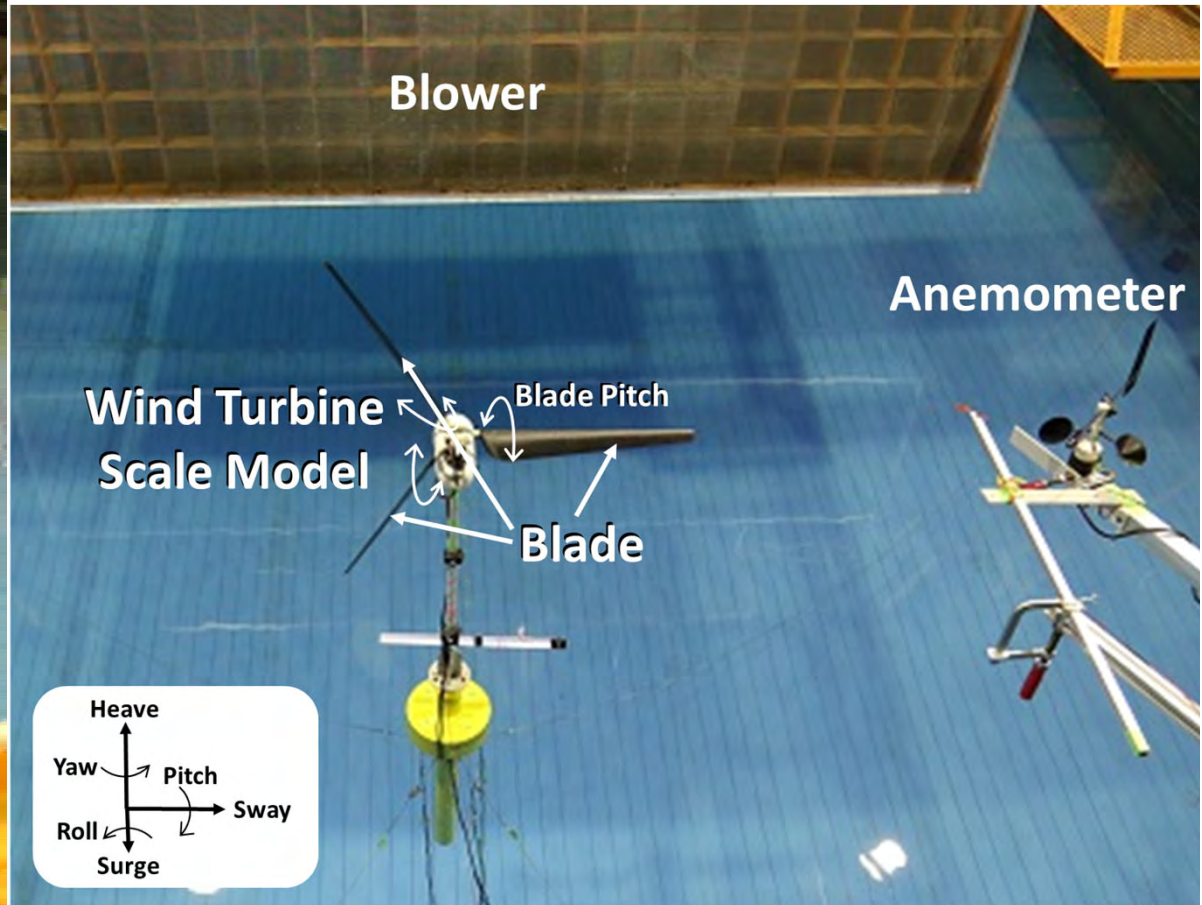
Introduction

- Blade pitch control for FOWTs
 - The platform (floater) is not fixed at the seafloor.
 - BP control affects not only the rotor's dynamics, but also **platform motions**. (both **aerodynamic torque** and **thrust force** change)
- Previous studies of advanced BP control for FOWTs
 - Simulation: H. Namik & K. Stol; *IEEE TCST* 2014, S.Raach et al.; *2014 ACC*, O. Bagherieh et al.; *2014 ACC*, B. Shahsavari et al.; *2016 ACC*, etc.
 - **Experiment**: N. Hara et al; *Wind Energy*, 2017
 - 1/100 scale model of a 5MW FOWT was used. H^∞ controller designed.
 - Problems: Uncertainty and integral action were not considered.
- **This study**
 - Design a BP controller using H^∞ loop-shaping design procedure.
 - Based on the loop-shaping concept. Integral action is easily incorporated.

FOWT Scale Model



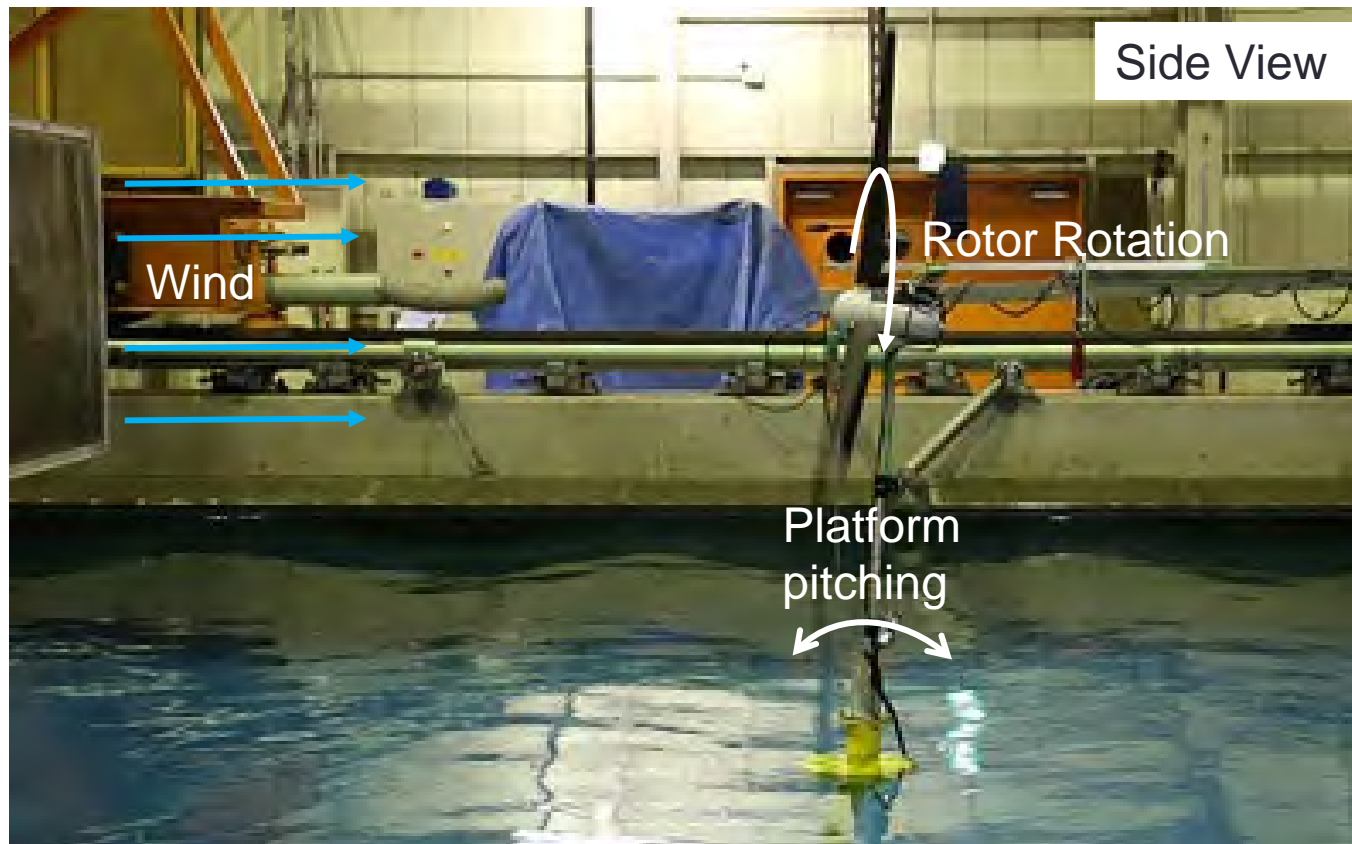
1/100 Scale Model of a 5MW wind turbine.



Experimental setup.
(Water tank facility, the Univ. of Tokyo)

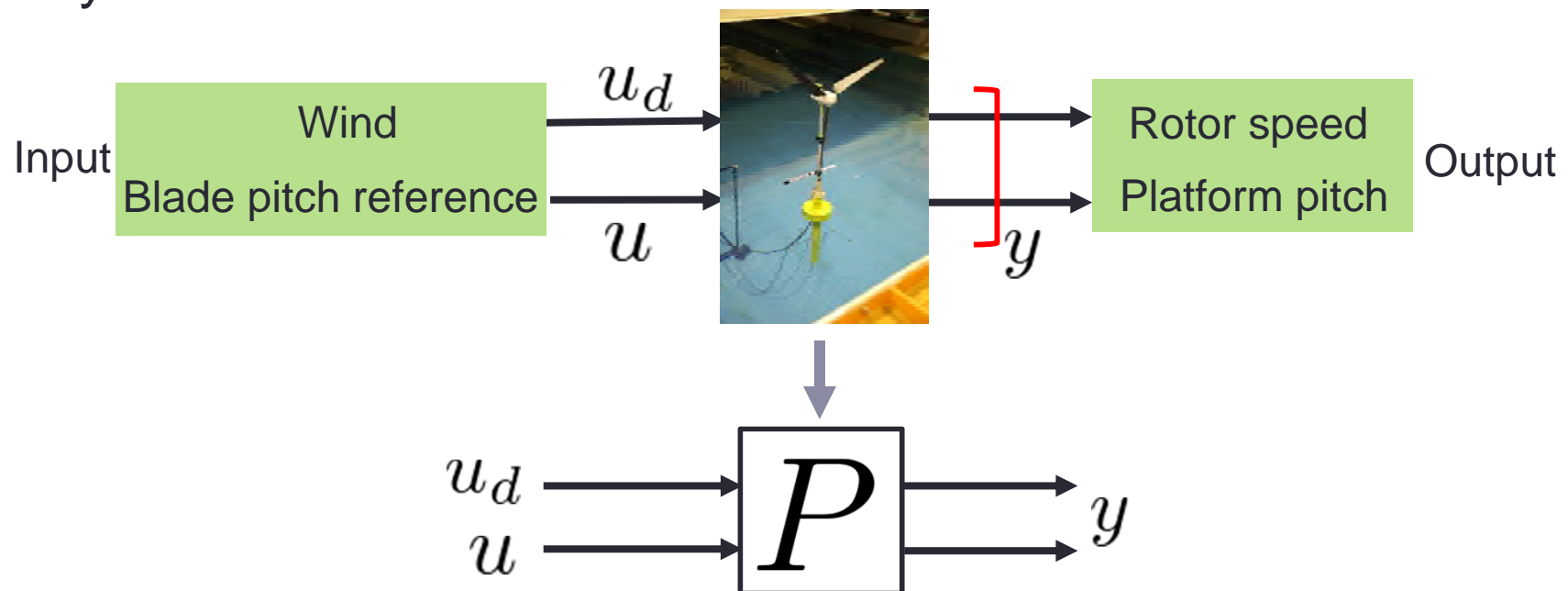
FOWT Scale Model

- Control Objective
 - Keep the rotor speed at 1.8Hz and suppress platform pitch fluctuations by the collective blade pitch control.

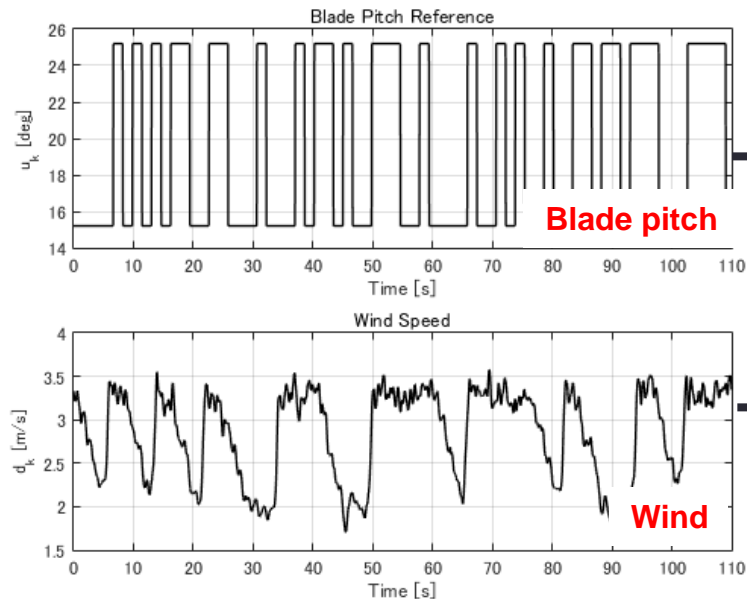


Nominal Model and Controller Design

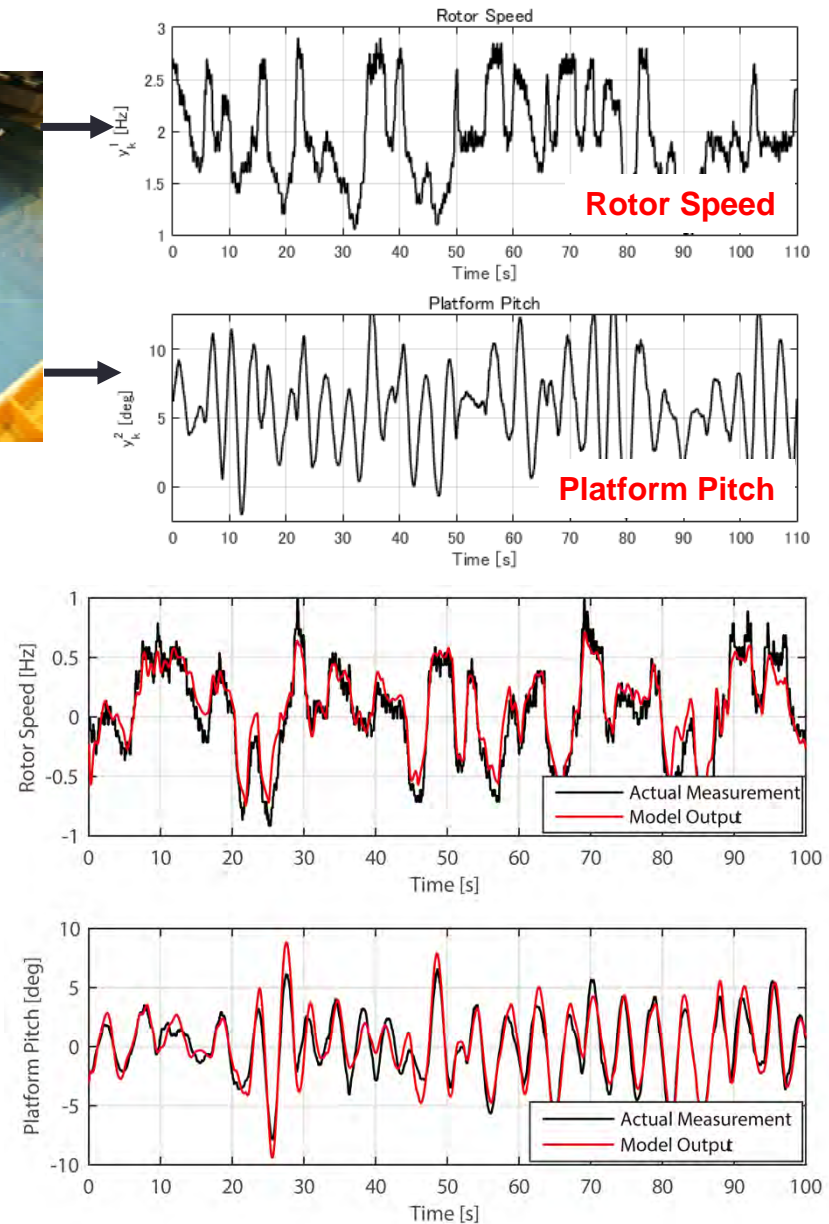
- Create a linear model around an operating point:
 - Wind speed: 2.7 m/s
 - Blade pitch angle: 20.20 deg
 - Rotor speed: 1.8 Hz
 - Platform pitch angle: 5.25 deg
- System identification



Identification Input



Output



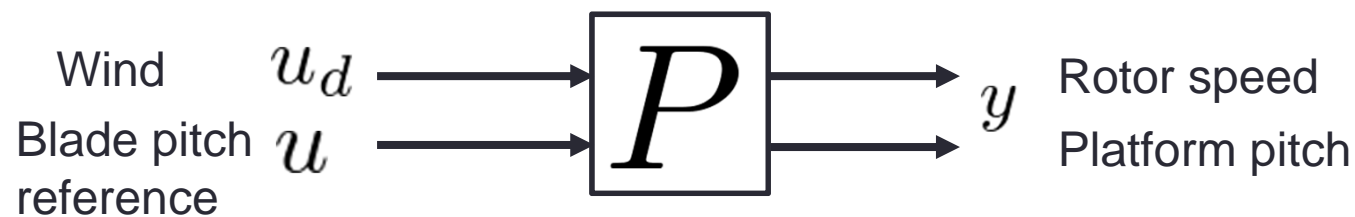
- System Identification
 - Obtain a set of input and output signals.
 - Subspace ID method
- Results
 - Fourth-order LTI system ($dT = 0.04$)
 - Validation test

Controller Design by H^∞ LSDP

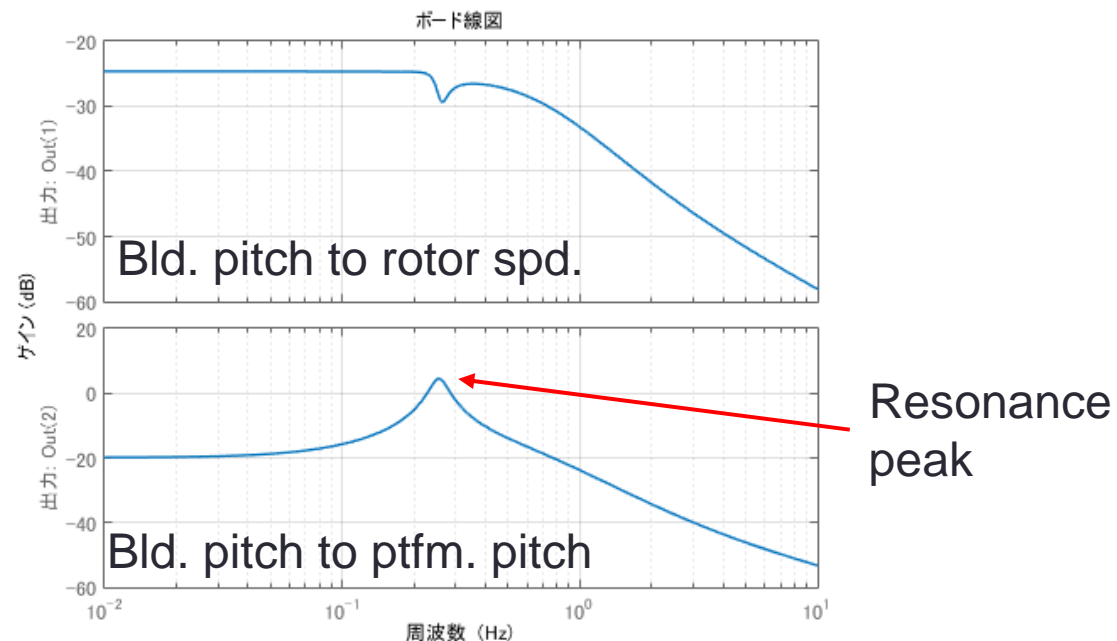
- Continuous-time nominal model for controller design

$$\dot{x}(t) = Ax(t) + Bu(t) + Dv(t)$$

$$y(t) = Cx(t)$$

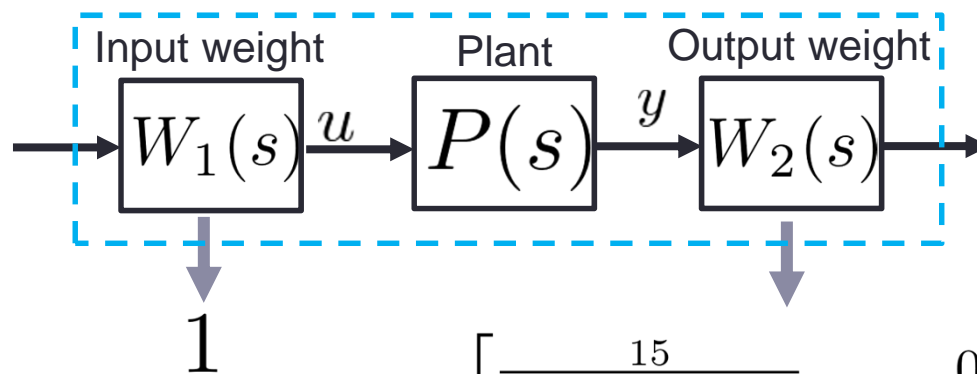


Frequency Response
(Gain characteristics)

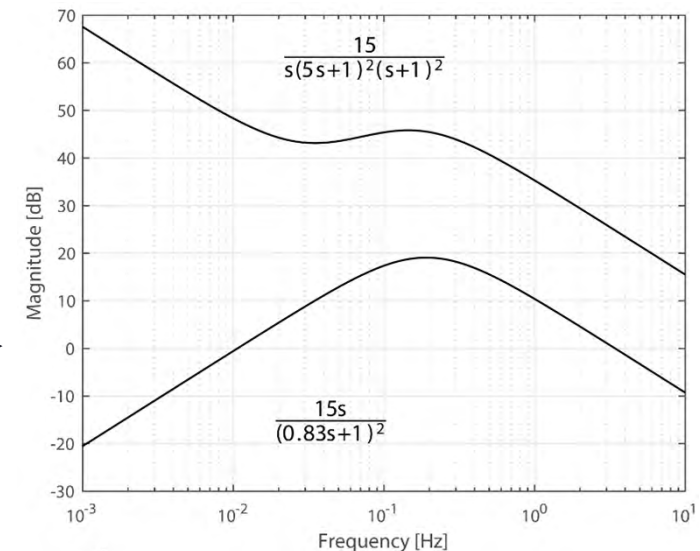


Controller Design by H^∞ LSDP

- H^∞ Loop-Shaping Design Procedure (LSDP)
 - Robust control design method
 - Based on the (classical) loop-shaping concept, guarantee robustness for a class of perturbations
- Design: choice of weighting matrices

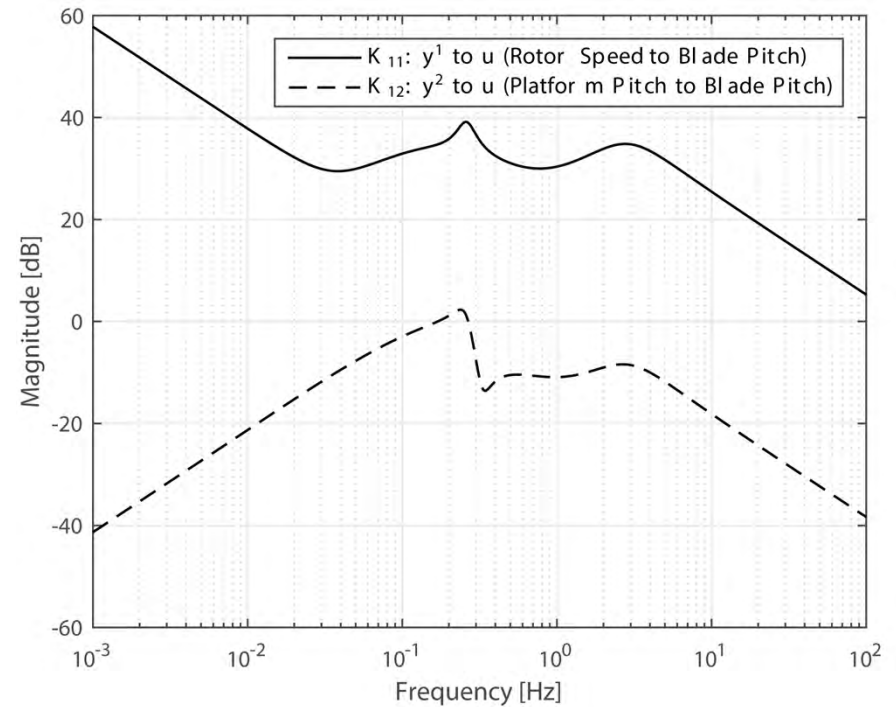
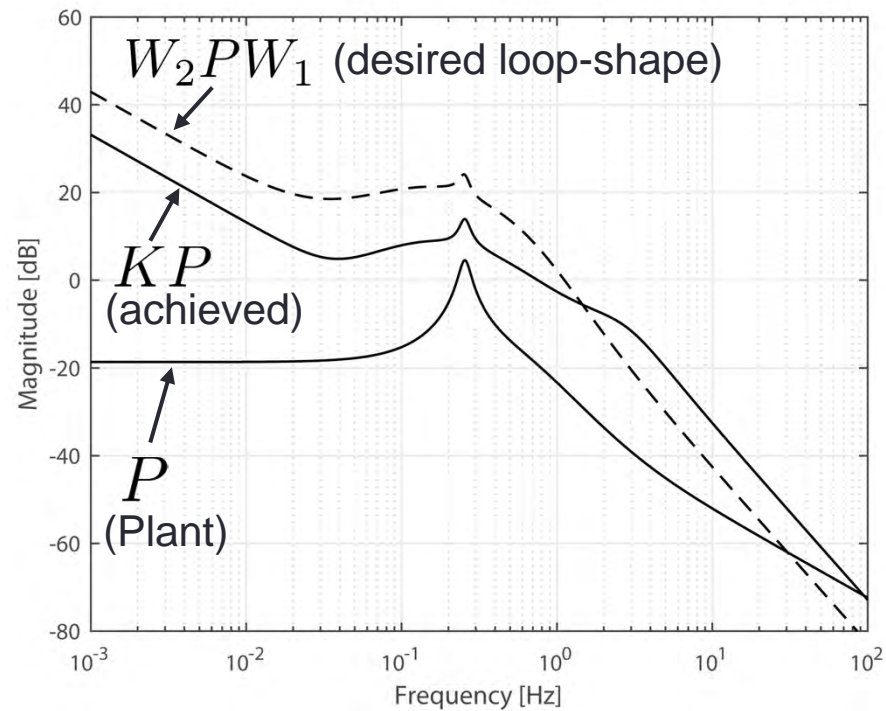


$$\begin{bmatrix} \frac{15}{s(5s+1)^2(s+1)^2} & 0 \\ 0 & \frac{15s}{(0.83s+1)^2} \end{bmatrix}$$



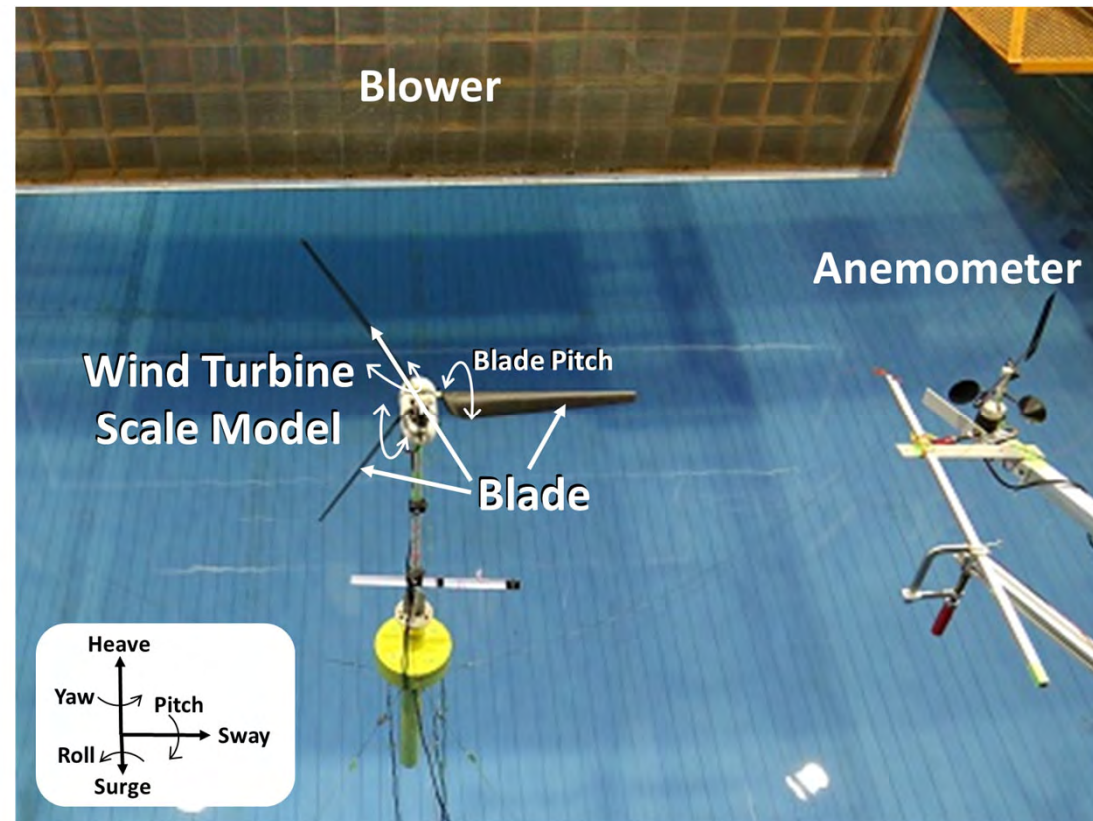
- Remark
 - Include an integrator (rotor spd. Output); resonance peak is suppressed (ptfm. Pitch)
 - The controller K was obtained ($\gamma = 3.2511$)

Controller Design by H^∞ LSDP



Experimental Results

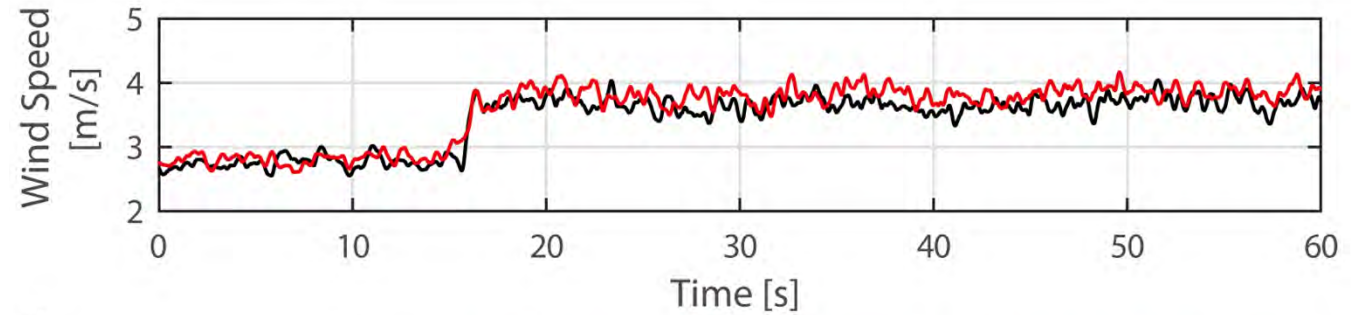
- Experimentally evaluated the effectiveness of the controller in terms of
 - Rotor speed regulation
 - Platform pitching suppression
- Designed controller
 - Implemented in PC with a sample time of 0.04 [s].



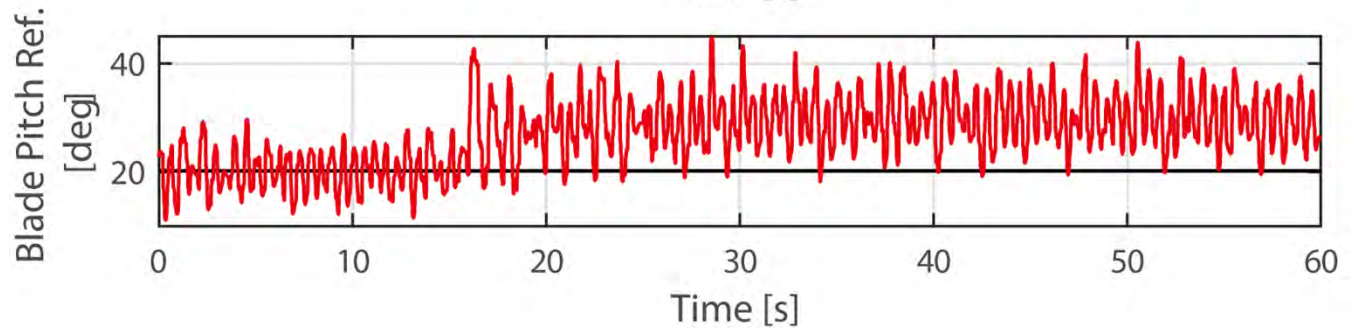
Experimental setup.
(Water tank facility, the Univ. of Tokyo)

Step wind change

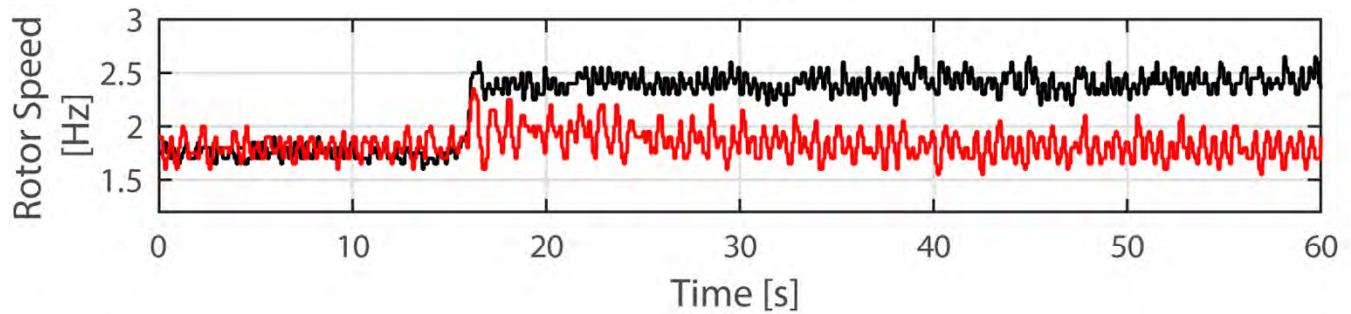
Wind



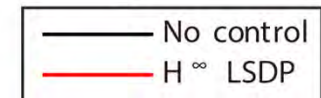
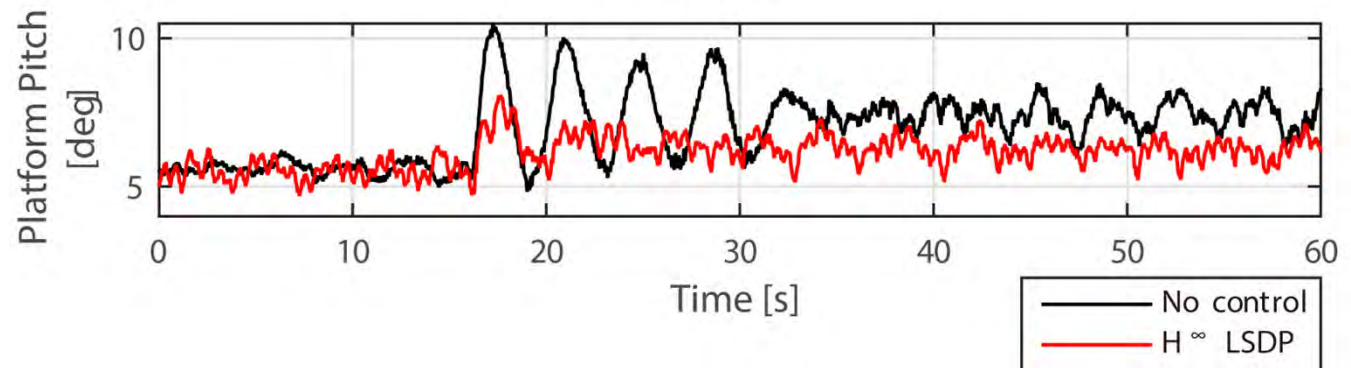
Blade pitch ref.



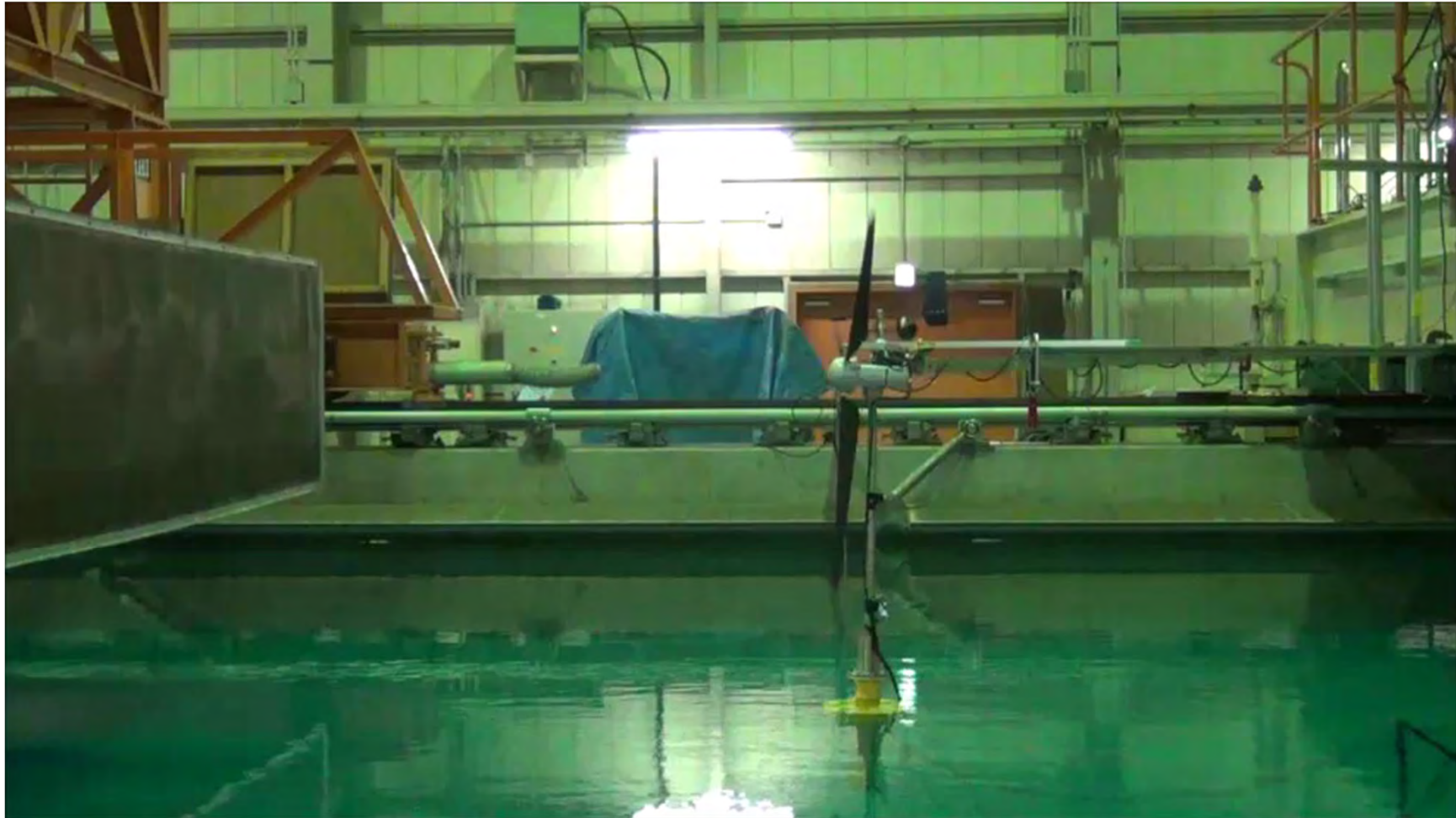
Rotor speed



Platform pitch

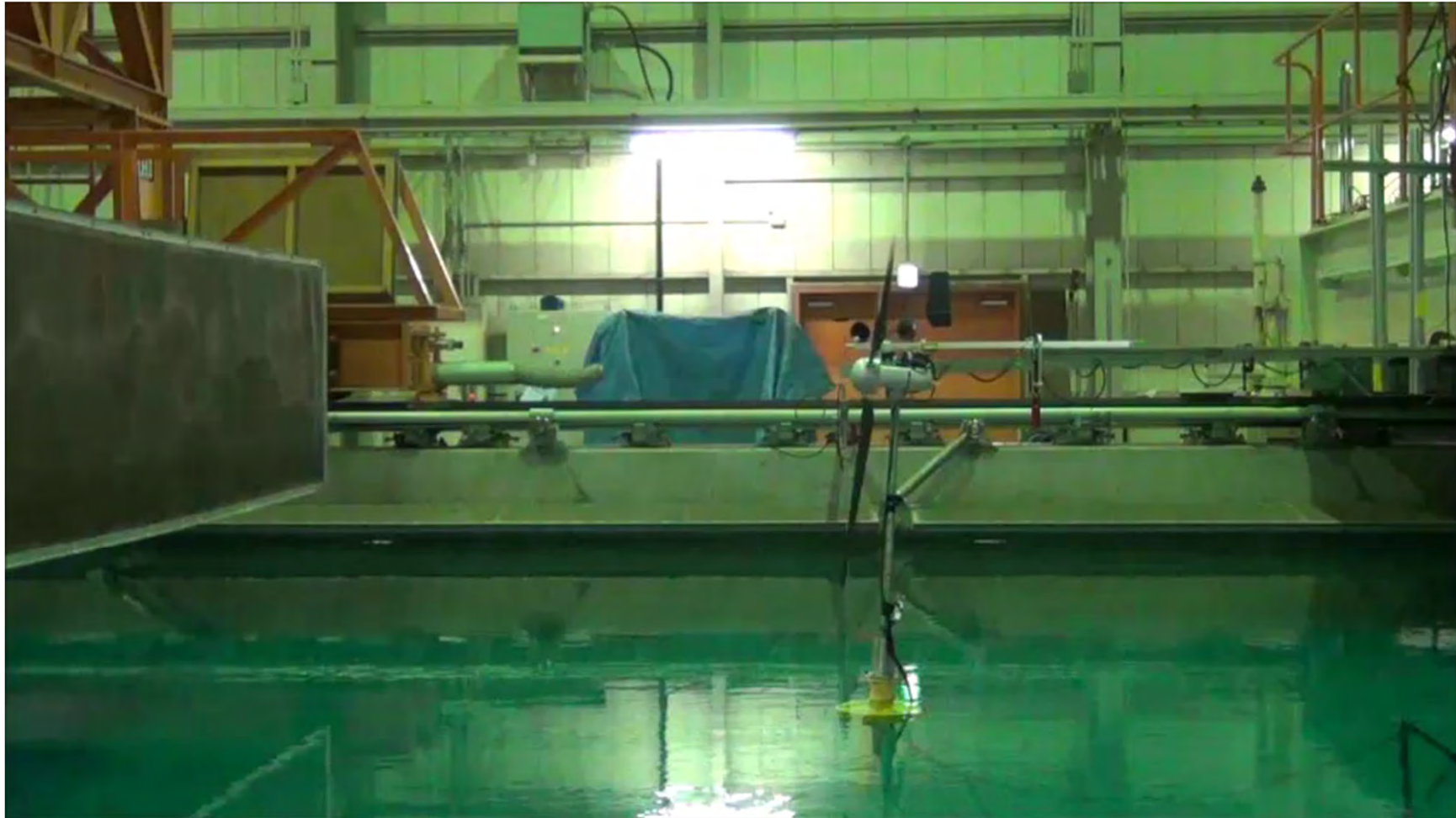


Result (const. blade pitch)



Movies are available at: <http://www.eis.osakafu-u.ac.jp/~n-hara/CCTA2017.htm>

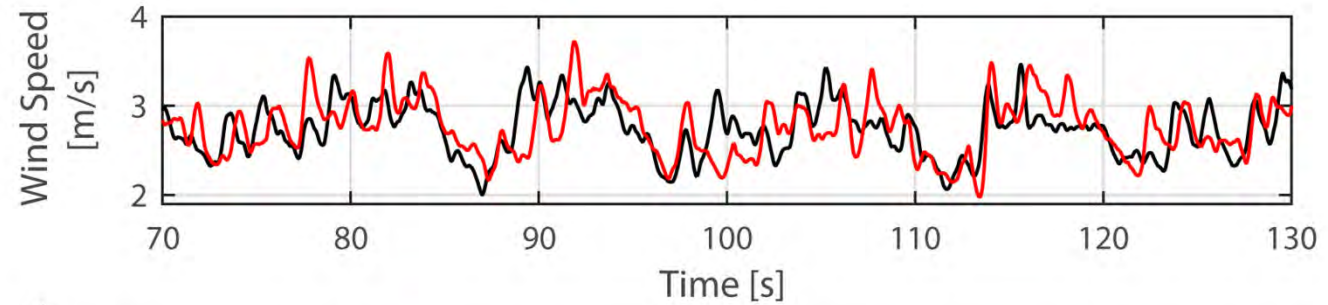
Result (designed H^∞ LSDP controller)



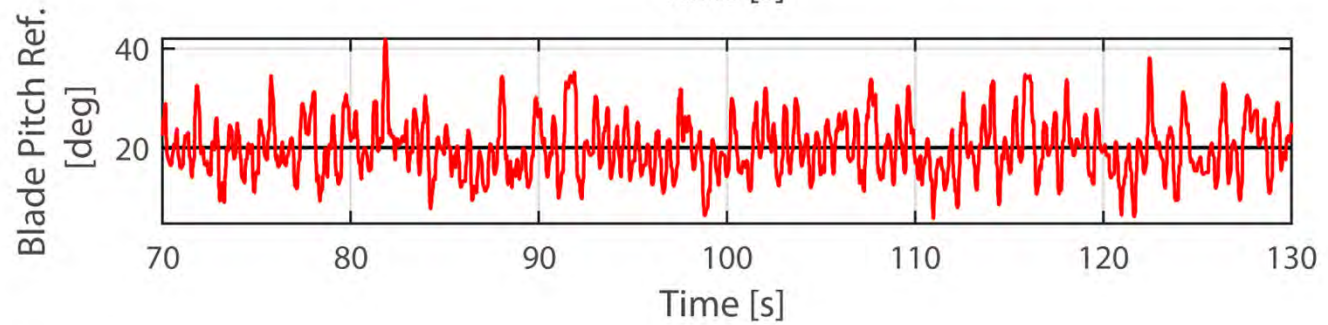
Movies are available at: <http://www.eis.osakafu-u.ac.jp/~n-hara/CCTA2017.htm>

Fluctuating Wind

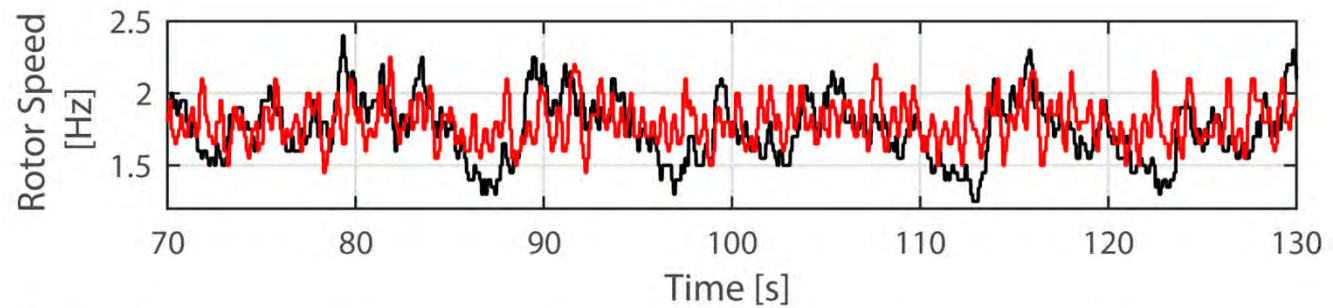
Wind



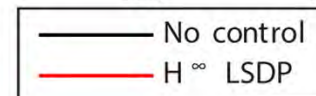
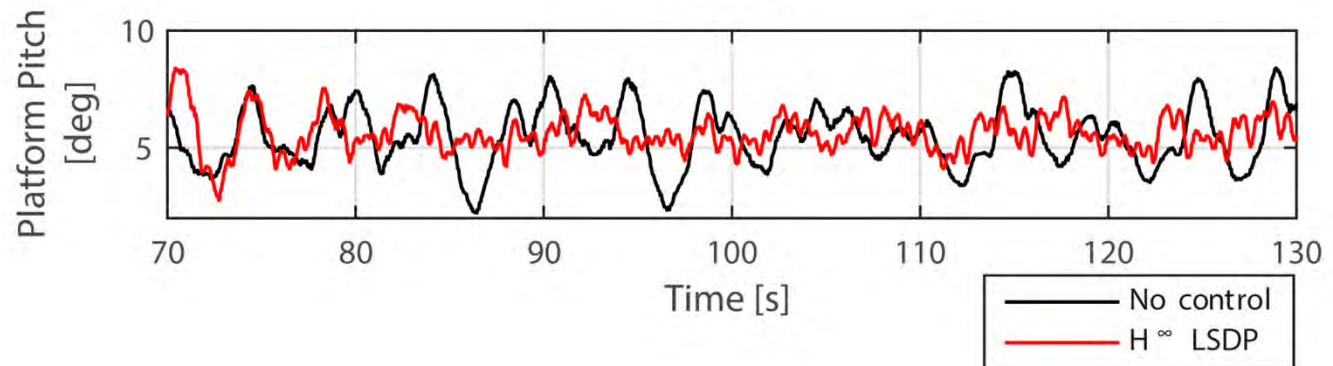
Blade pitch ref.



Rotor speed

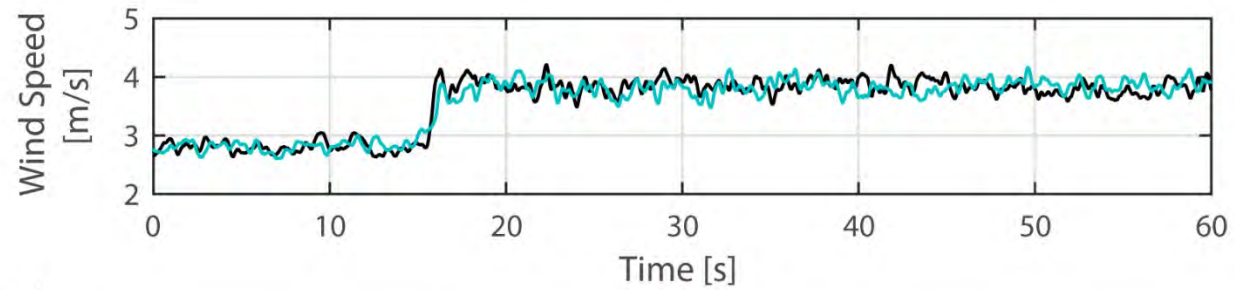


Platform pitch

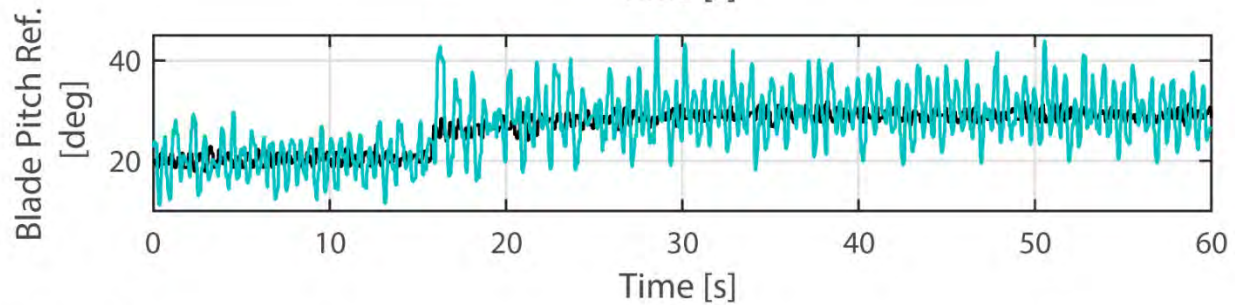


Comparison with PI

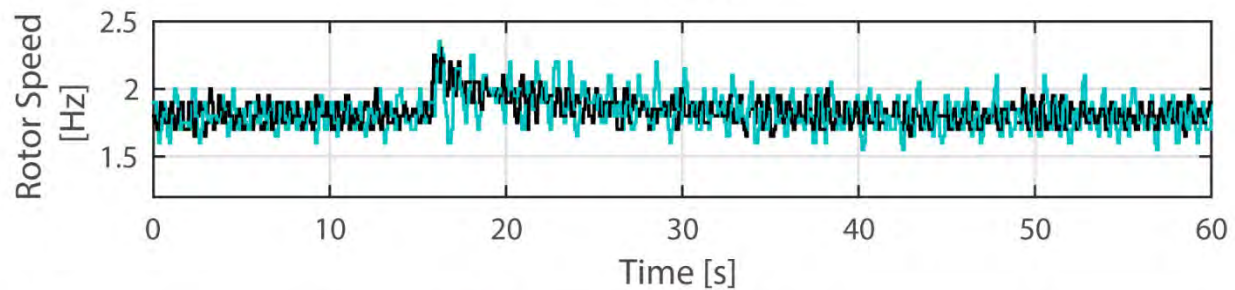
Wind



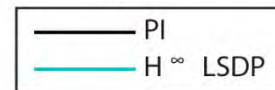
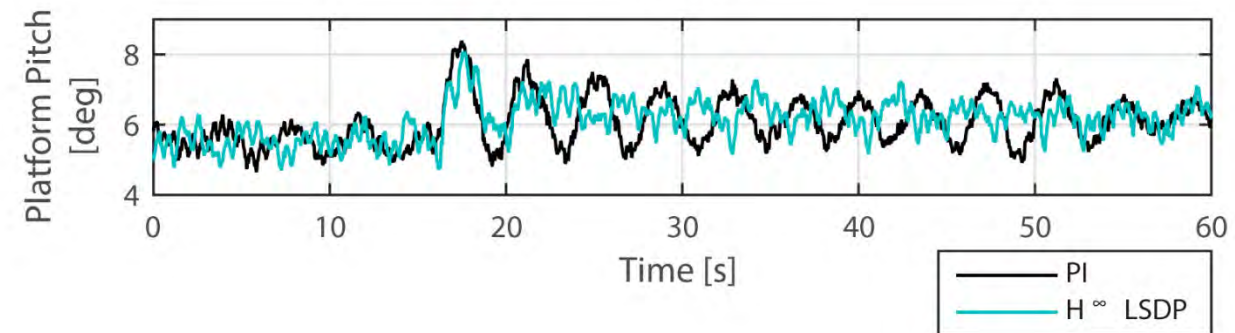
Blade pitch ref.



Rotor speed



Platform pitch



Concluding Remarks

- Designed a (collective) blade pitch controller
 - Plant: obtained by system identification
 - Controller: design by H^∞ LSDP
- We carried out the experiments
 - Platform pitching was suppressed.
 - Blade pitch reference tends to be large. Need some more tuning of the weights.
- Future research topics
 - Evaluation of fatigue loads (tower base, blade root, etc)
 - LTV identification
 - Comparison with the behavior of the corresponding full-scale model.
 - Individual blade pitch control (in progress, currently fabricating a scale model.)



Acknowledgement

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Contact

Please feel free to contact me if you have any questions:

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